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# Dilatometric study of the $\text{ZnTiO}_3$ phase transition kinetic influenced by nano powder sintering

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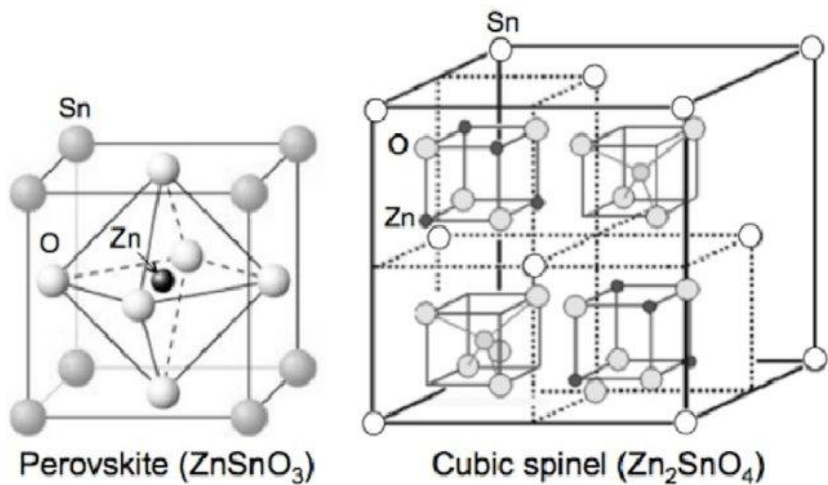
**Nebojša Labus<sup>1</sup>,**

**Milena Rosić<sup>2</sup>,**

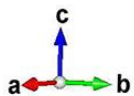
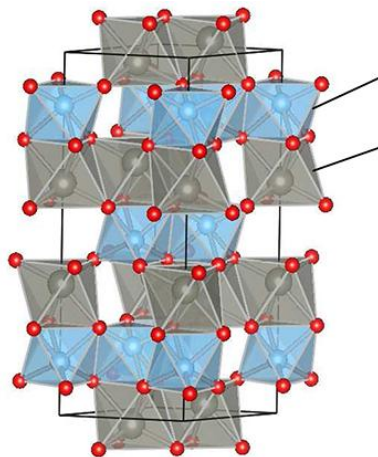
**Smilja Marković<sup>1</sup>,**

**Maria-Vesna Nikolić<sup>3</sup>**

# Phase transition $\text{ZnTiO}_3$ to $\text{Zn}_2\text{TiO}_4$

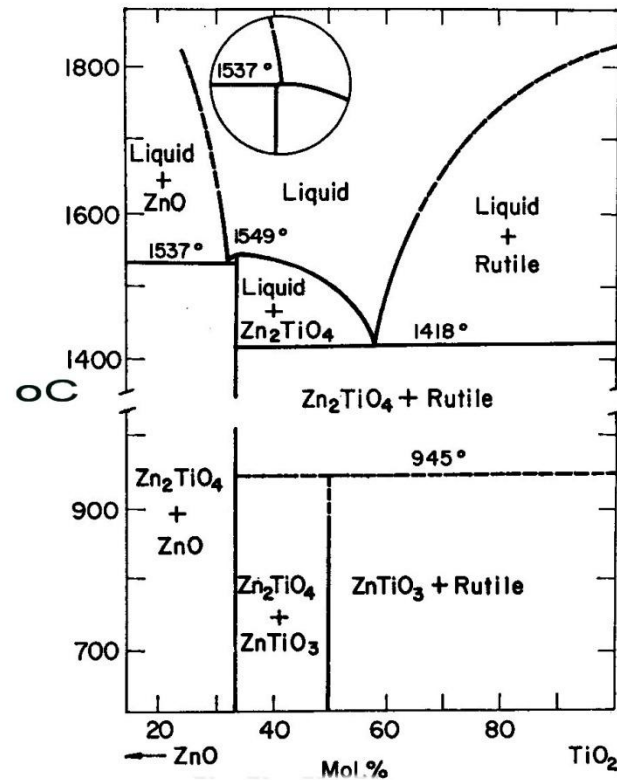


$$r = \frac{r_A + r_X}{\sqrt{2}(r_B + r_X)}$$

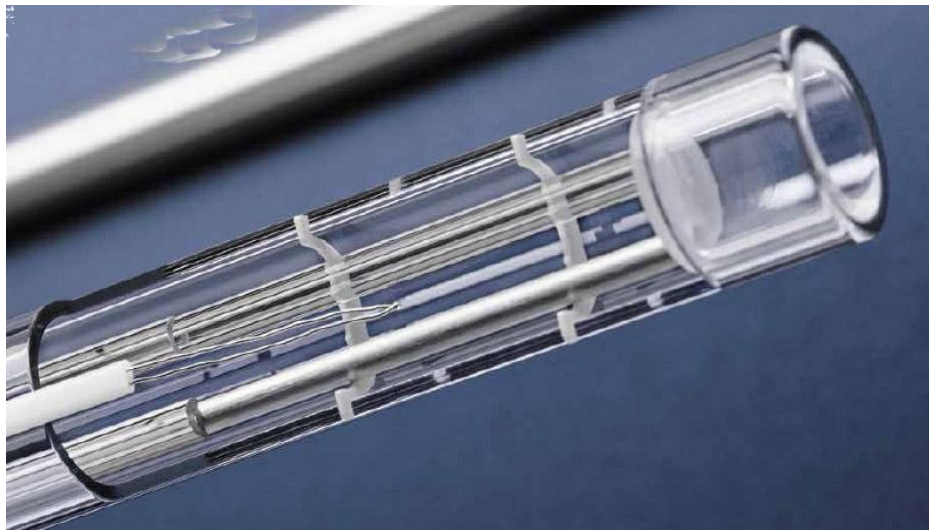


(a) Ilmenite-type

$\text{ZnO-TiO}_2$



F. H. Dulin and D. E. Rase, *J. Am. Ceram. Soc.*, **43** [3] 130 (1960).

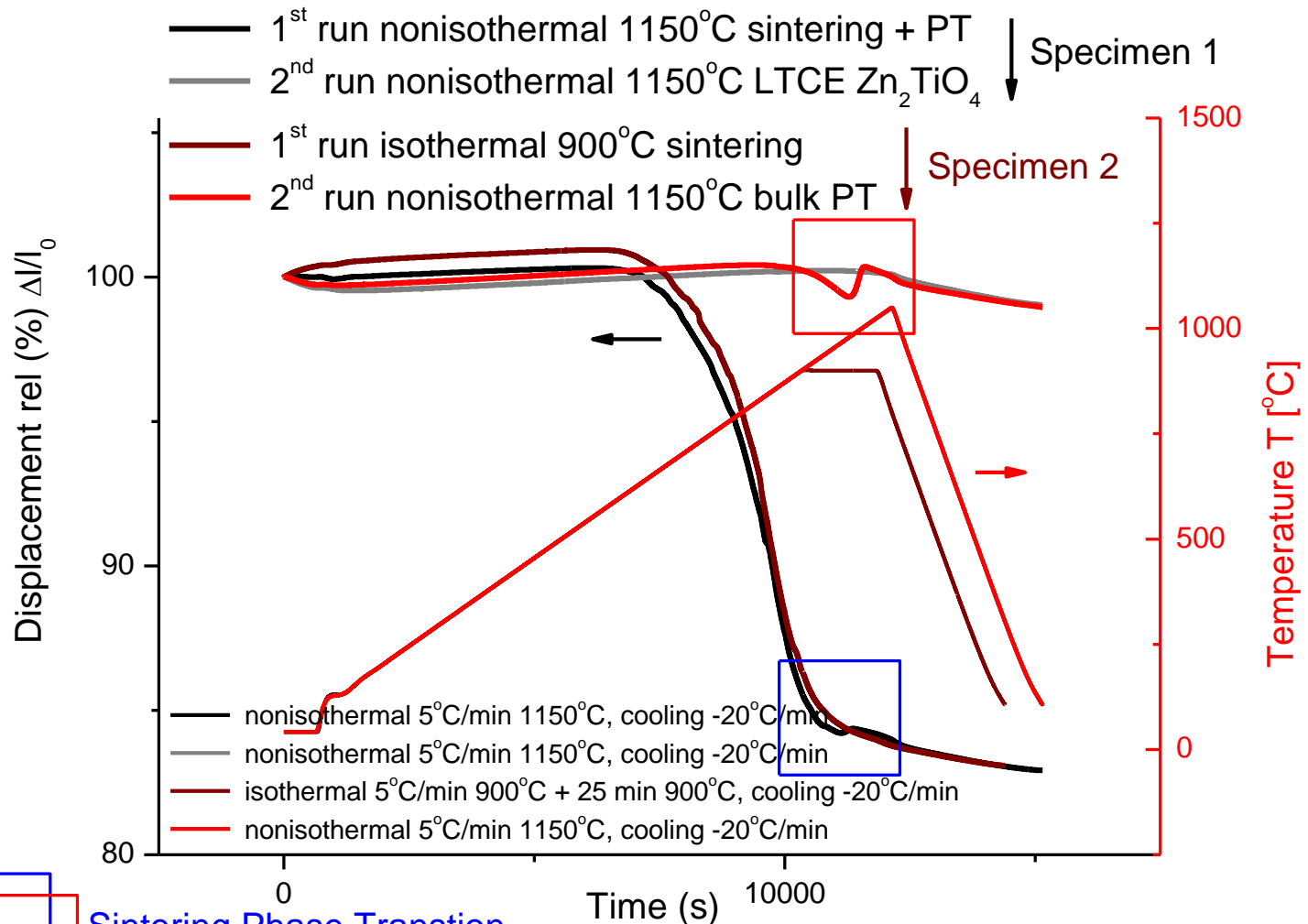


# Experiment

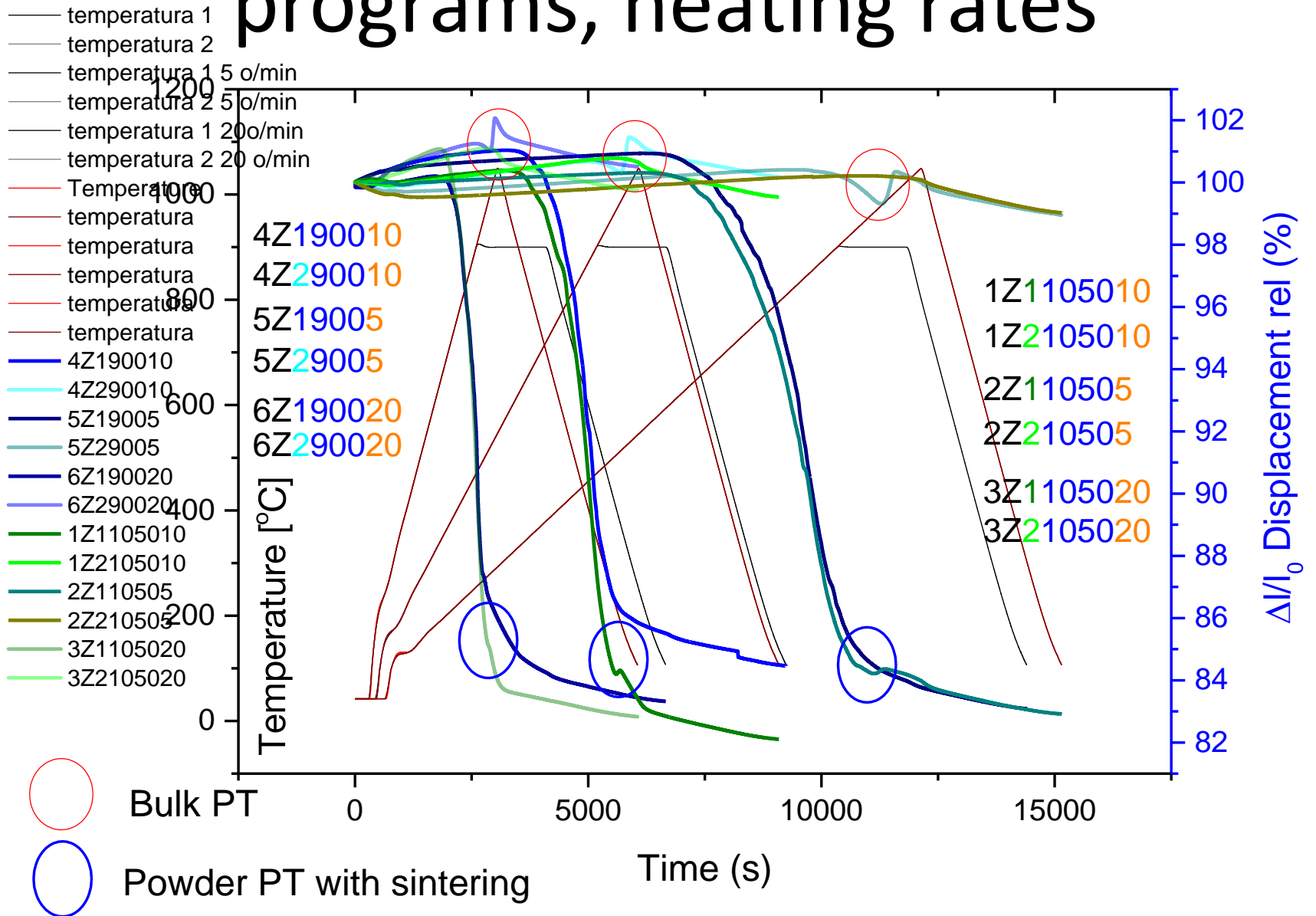


# Phase transition $\text{ZnTiO}_3$ to $\text{Zn}_2\text{TiO}_4$

## Experimental setup

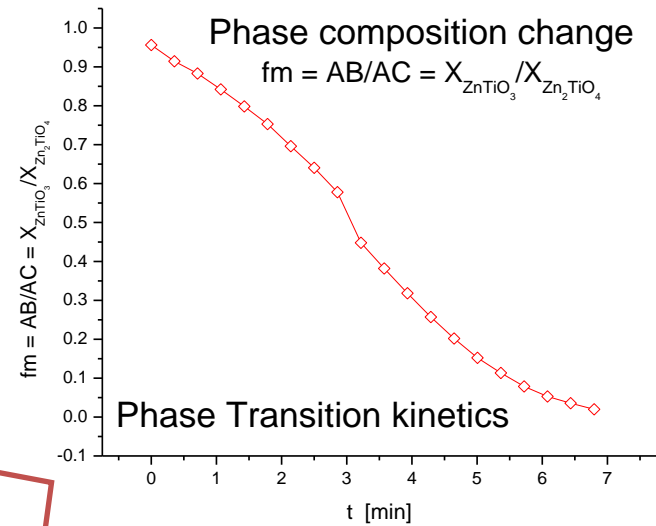
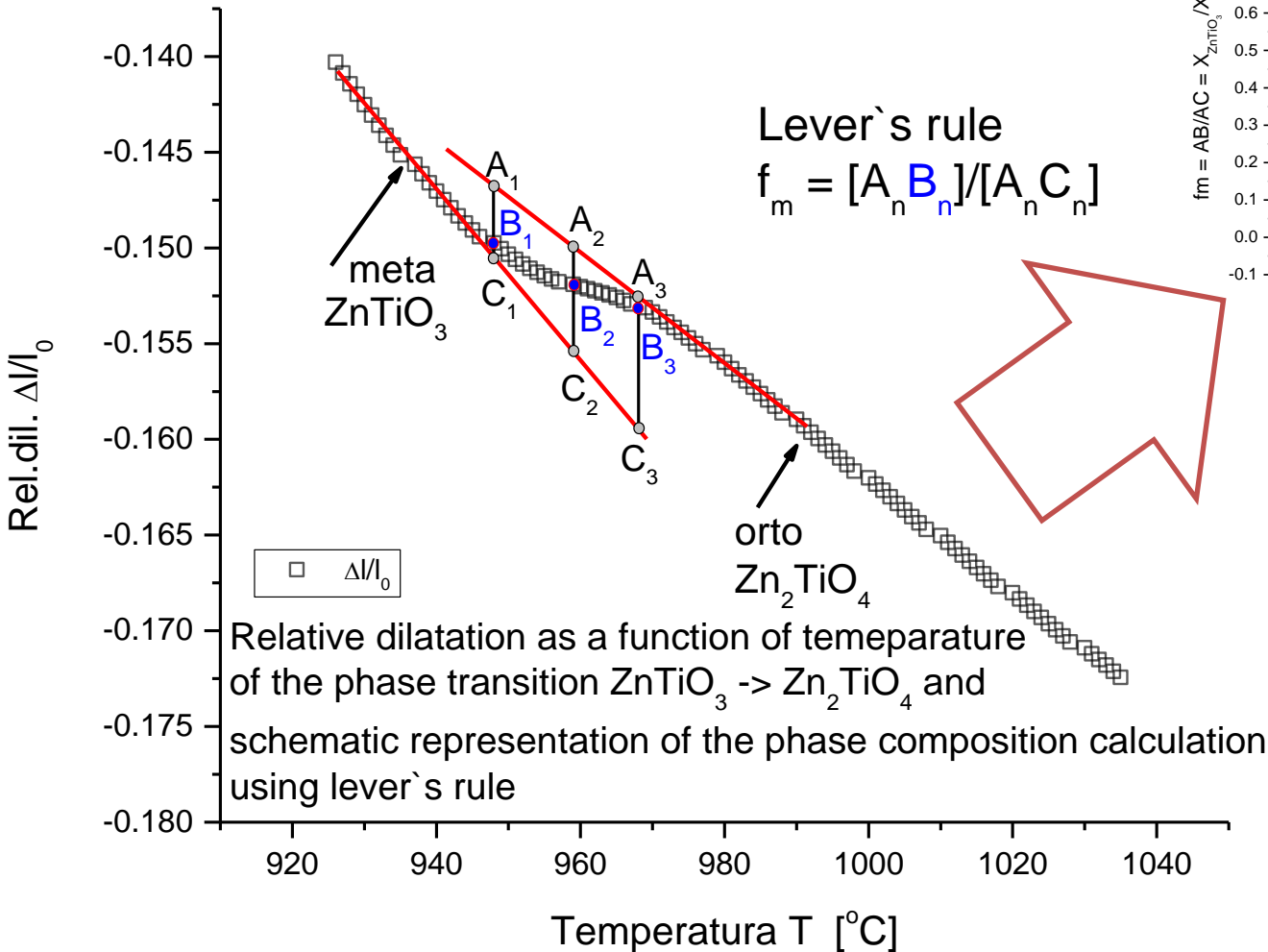


# Dilatometric curves and temperature programs, heating rates

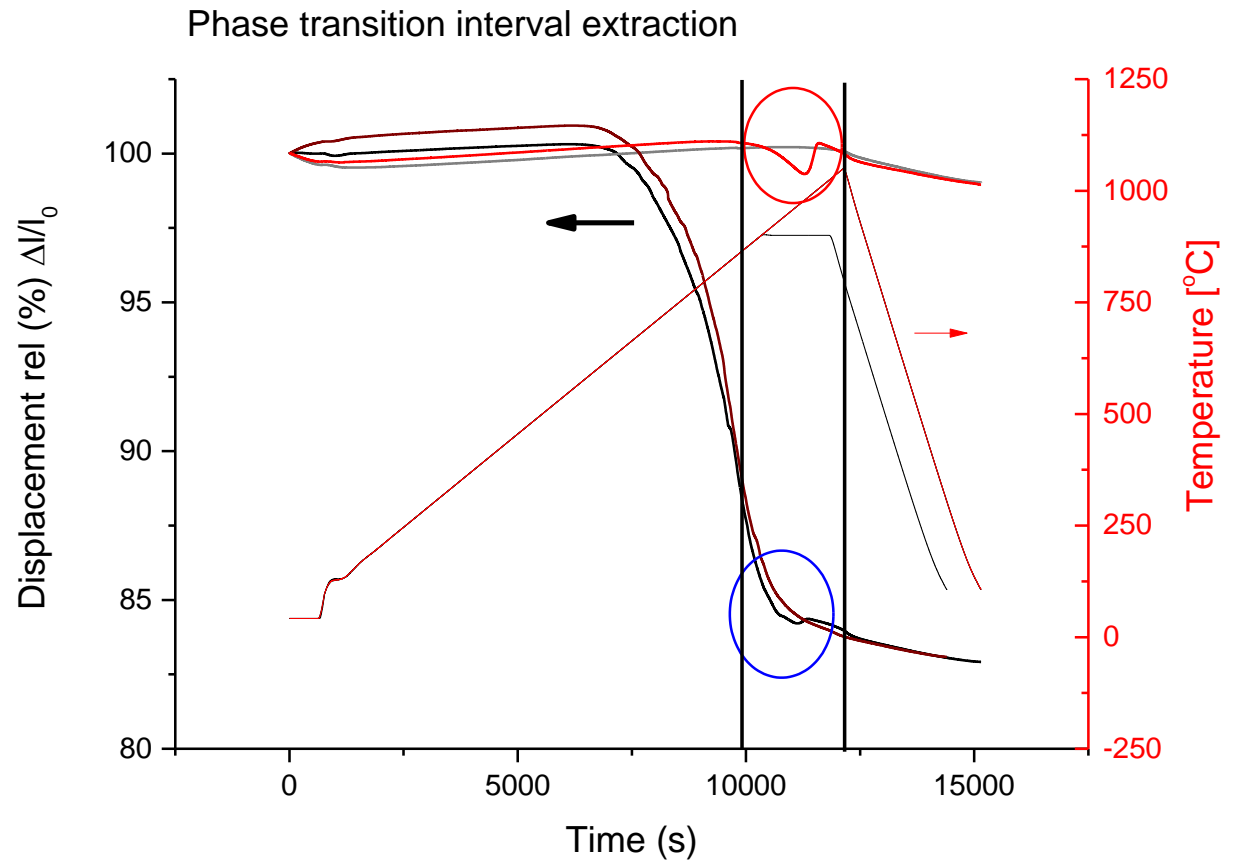
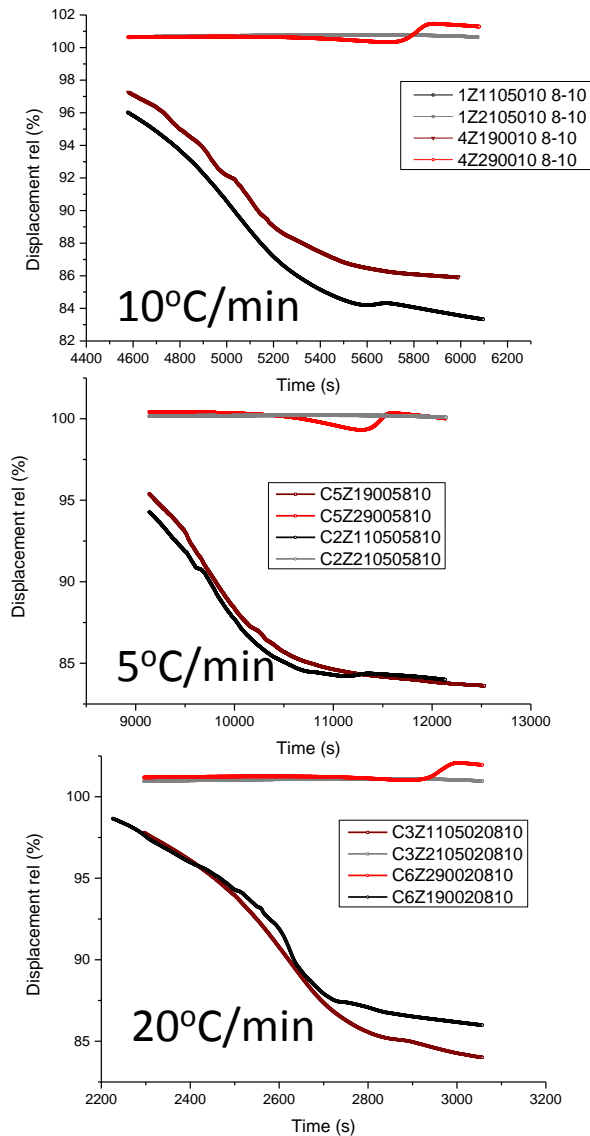


# Aim

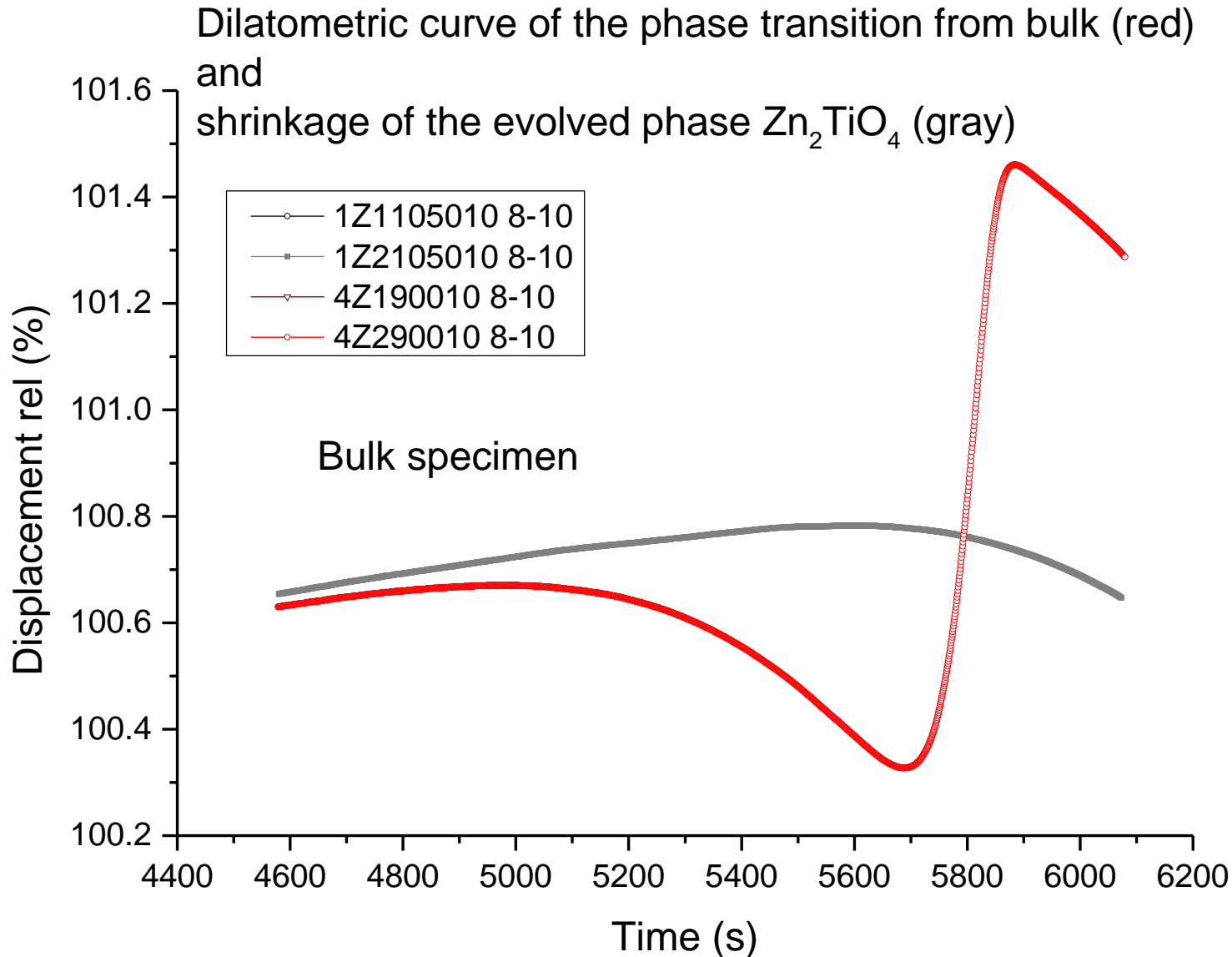
## Phase transition kinetics



# Phase transition interval extraction

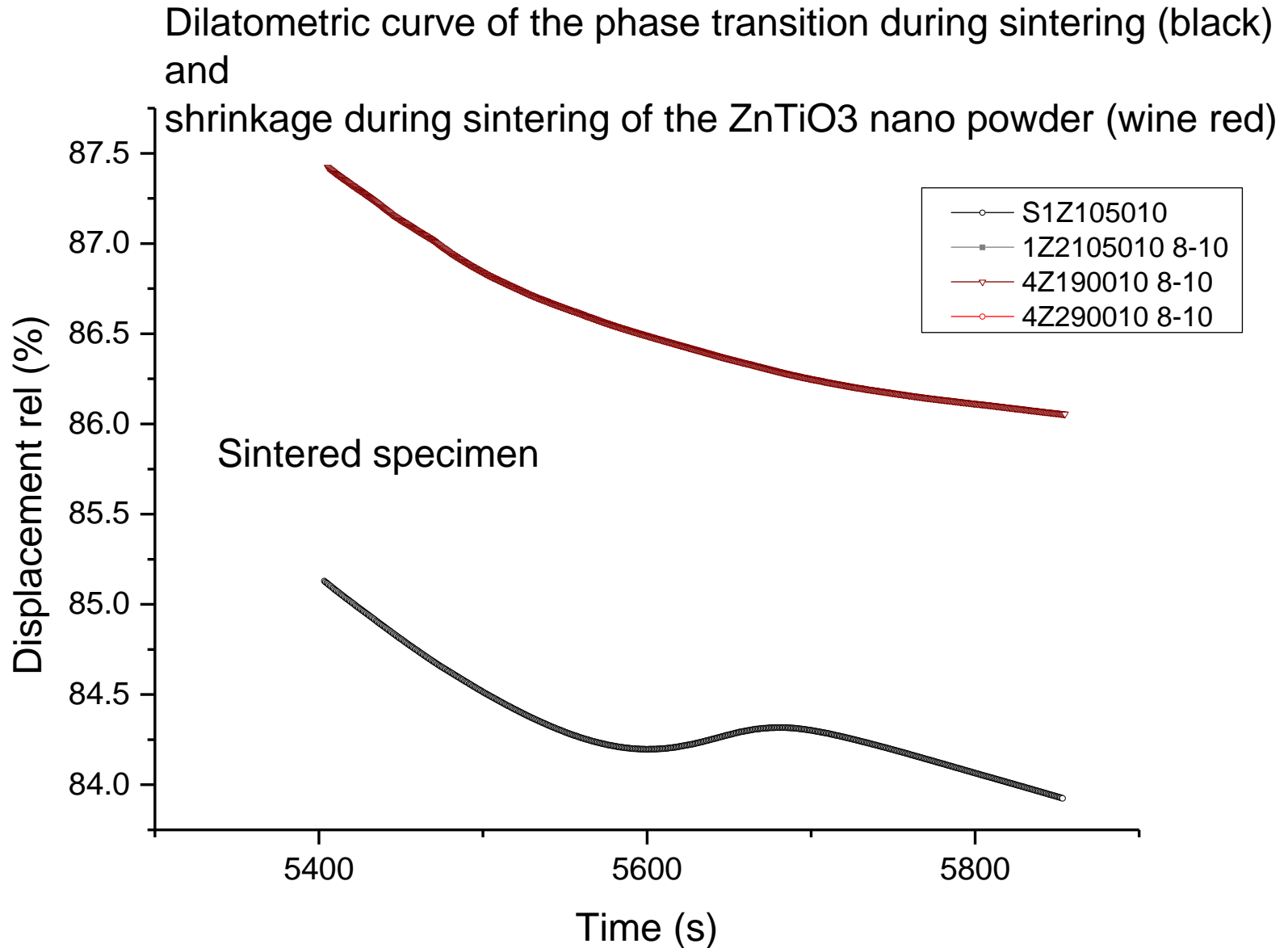


# Bulk phase transition dilatation

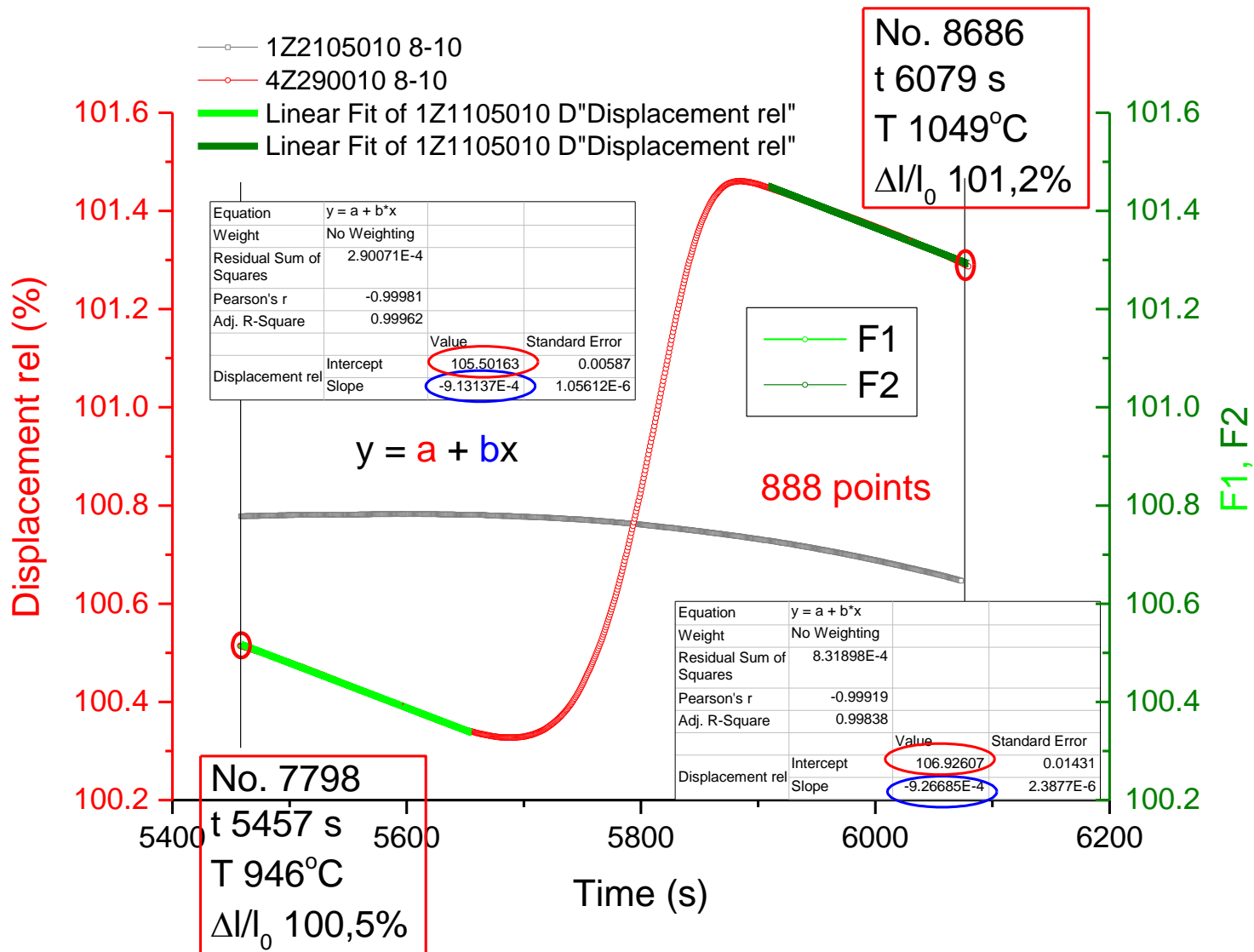




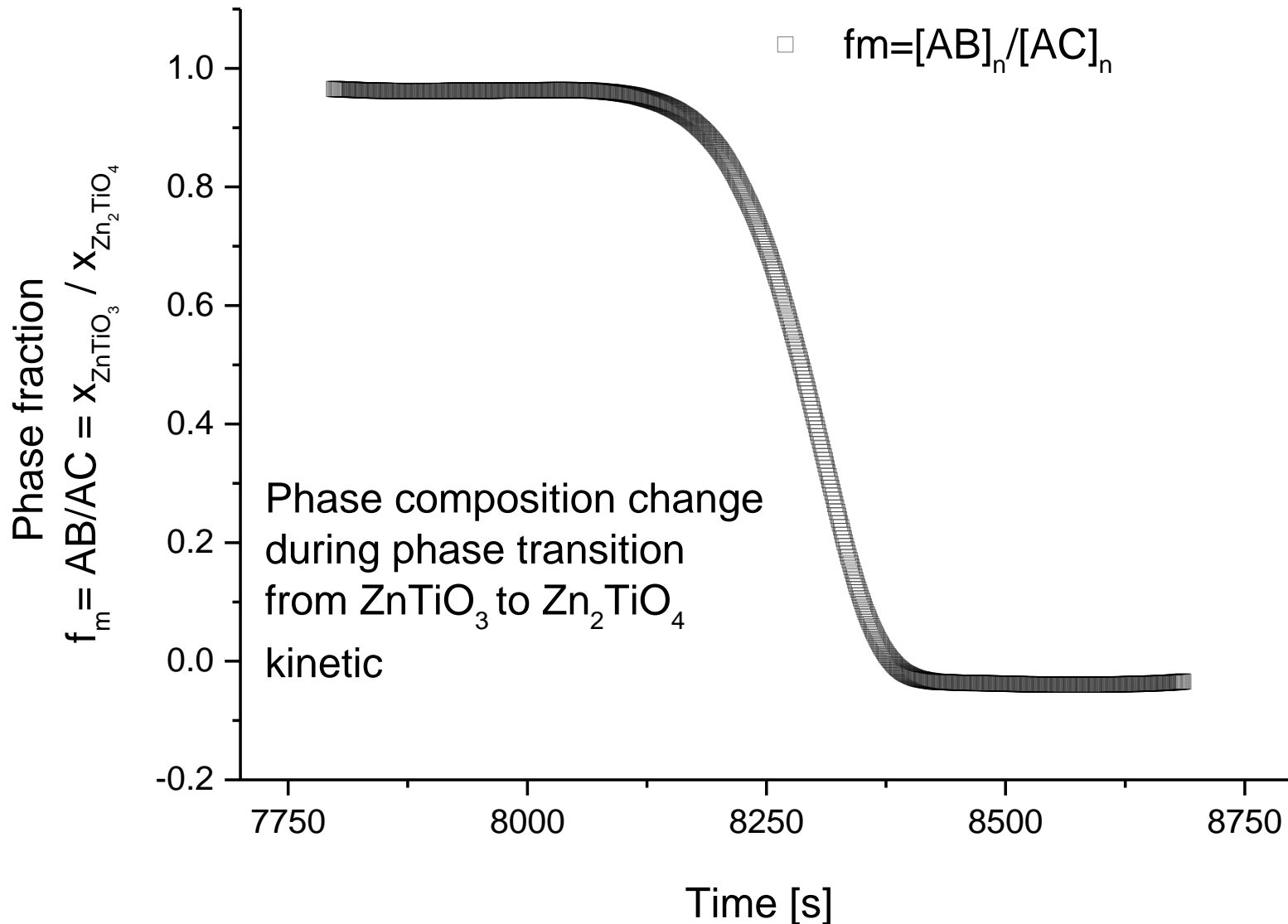
# Sintering phase transition dilatation



# Linear fitting and interpolation of the inserted linear functions

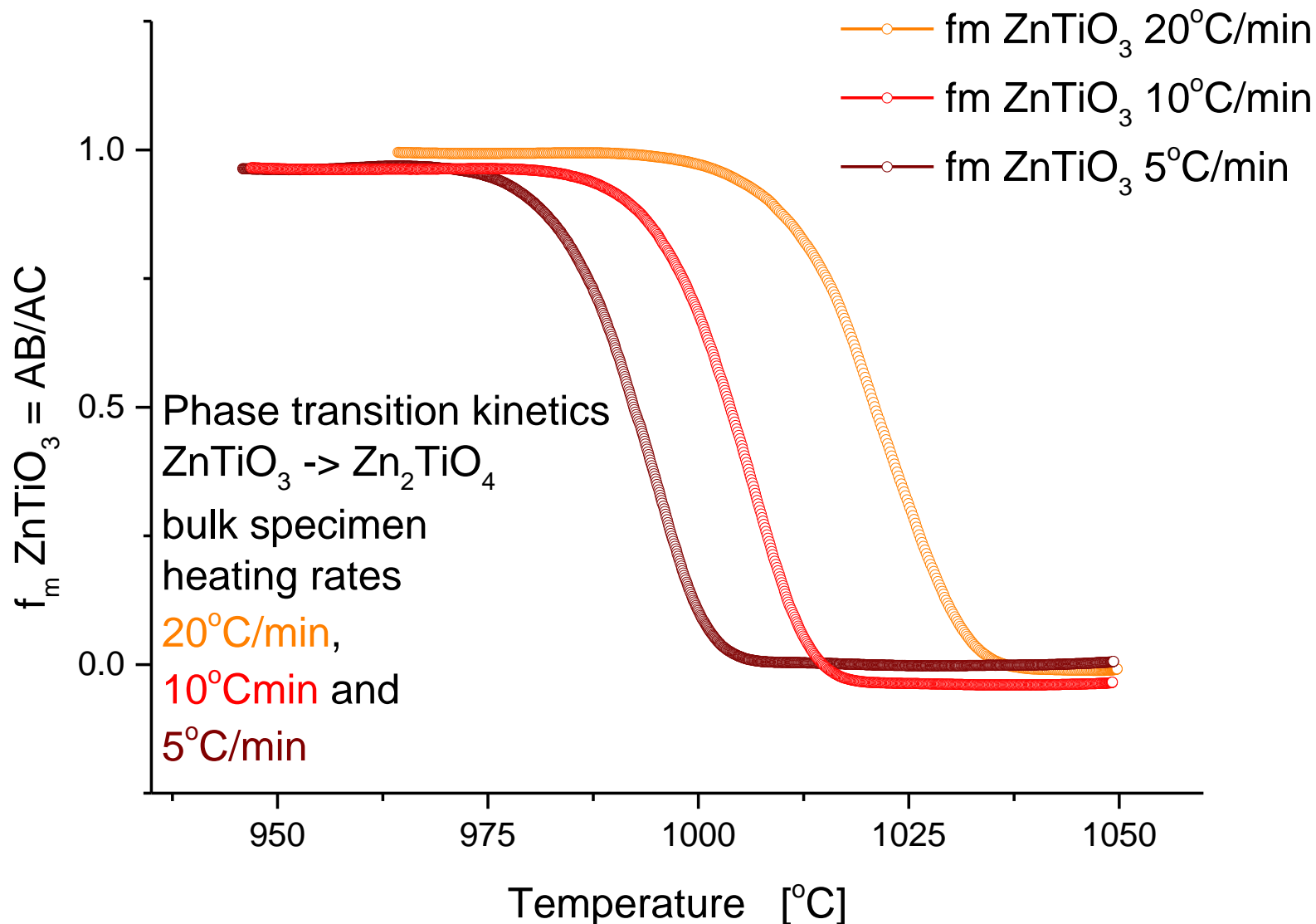


# Phase composition - kinetic

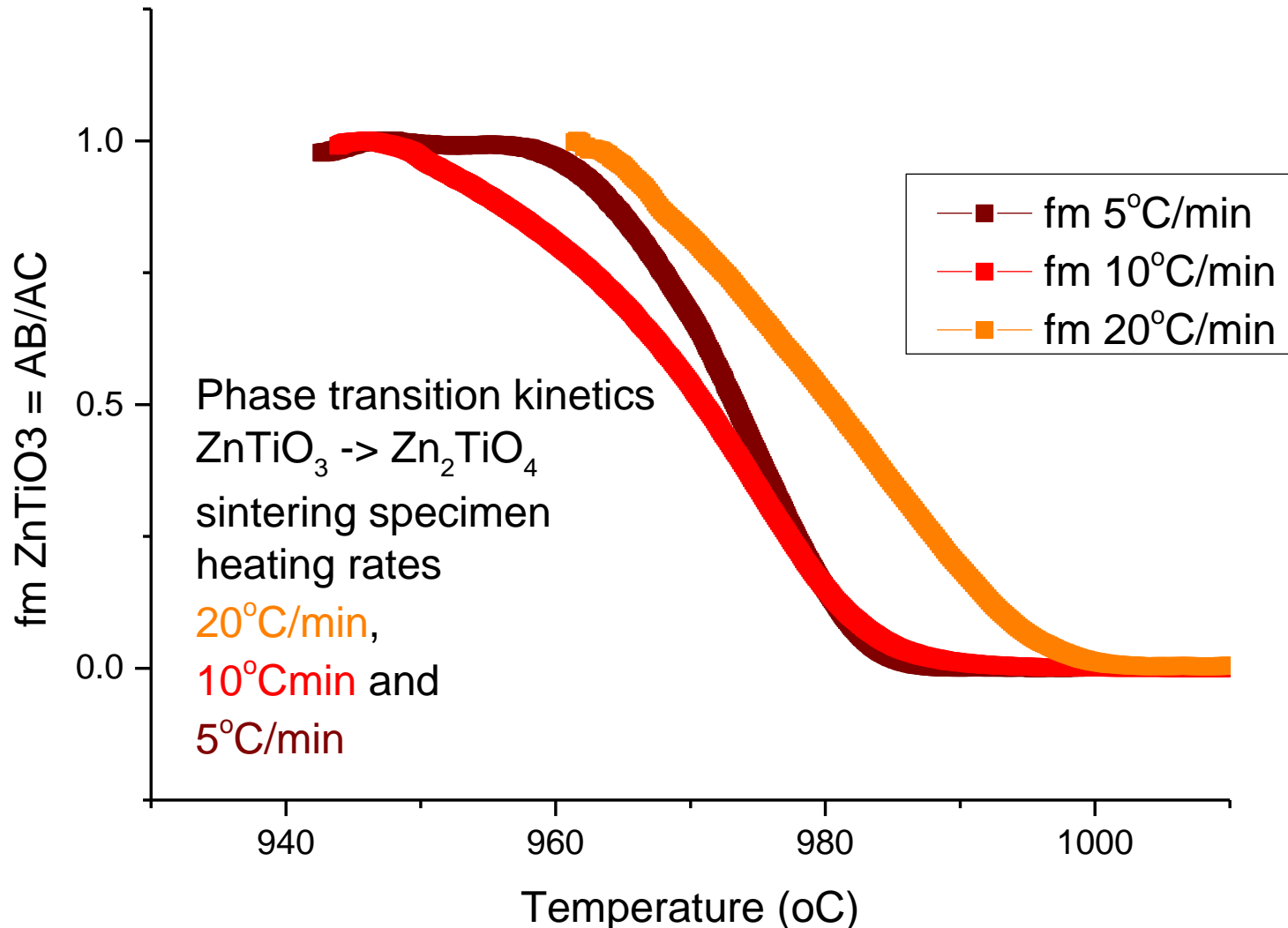


# Phase transition from bulk specimen

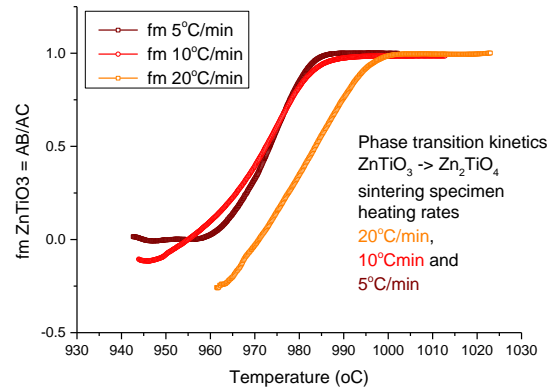
## Three heating rates



# Phase transition from sintered specimen - Three heating rates



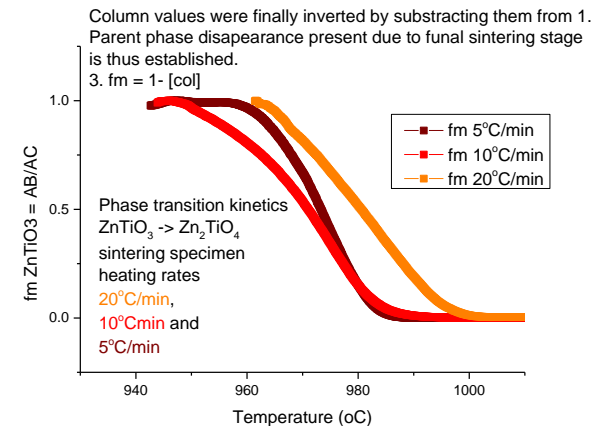
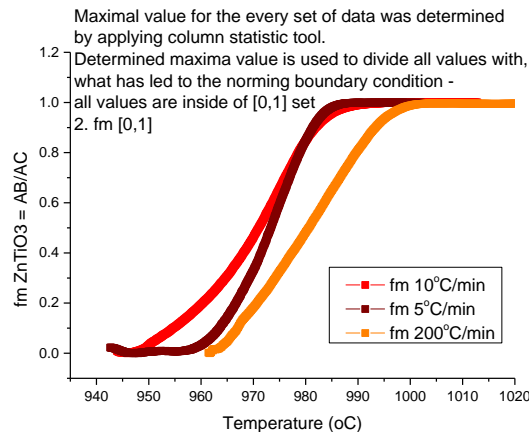
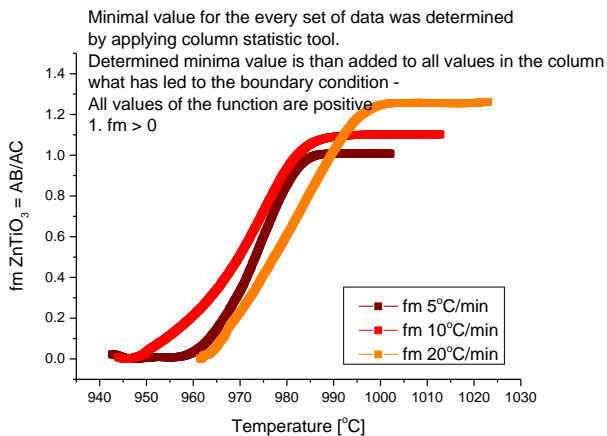
# Mathematical procedures enabling comparison of the data



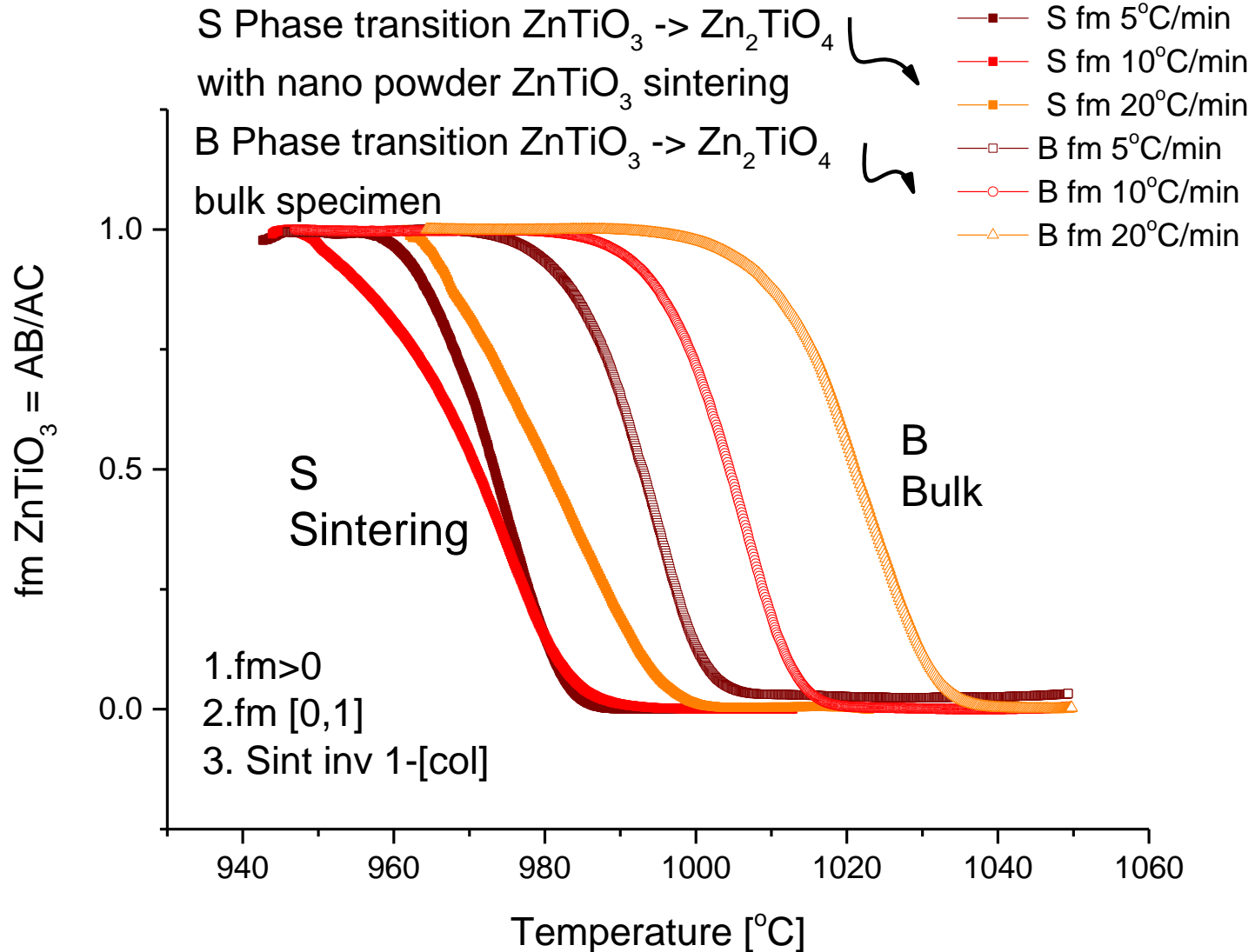
1.  $fm > 0$

2.  $fm [0,1]$

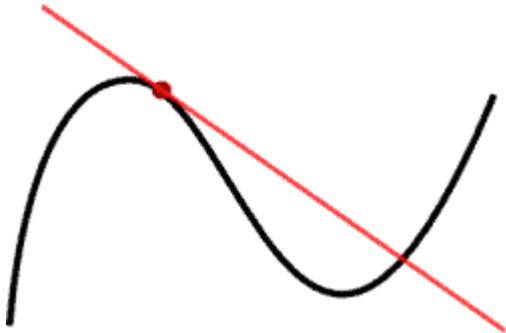
3.  $fm = 1 - [col]$



# Phase transition kinetics comparison: Bulk and Sintered - Experimental



# Correction Calculus



$\frac{d}{dx} \left[ \frac{f(x)}{g(x)} \right] = \frac{g(x)f'(x) - f(x)g'(x)}{g(x)^2}$ 
 $F = mg = ma = m \frac{dh}{dt}$ 
 $m \frac{d^2x}{dt^2} = -kv$

$\frac{dx}{dt} = \frac{dy}{dx} = \frac{dy}{dx}$ 
 $y = mx + b$

$(\ln x)^2 = \frac{1}{2} \int \frac{1}{x} dx = \ln|x| + c$ 
 $\int \sin x dx = -\cos x + c$ 
 $\int_a^b f'(x) dx = f(b) - f(a)$

$x^2 - 3x - 4 = 0$ 
 $4x^2 - 5x - 1 = 0$

$\frac{dA}{dt} = \frac{dB}{dt} = -\frac{dC}{dt} = -\frac{dD}{dt} = (A_1)T^{\frac{1}{2}}AB - (A_2)T^{\frac{1}{2}}CD$

$x^2 = A \frac{dT}{dt} = (c_1) \frac{dA}{dt} - (c_2)(T_0 - T)$

$\left[ x + \frac{b}{2a} \right]^2 = \frac{b^2 - 4ac}{4a^2}$ 
 $x + \frac{b}{2a} = \frac{\sqrt{b^2 - 4ac}}{2a}$ 
 or  $x + \frac{b}{2a} = -\frac{\sqrt{b^2 - 4ac}}{2a}$ 
 $(x + t)h, f(x + t)$

$\frac{d}{dx} \int_a^x f(t) dt = f(x)$ 
 $\frac{d^2c}{dt^2} = -kv - f \frac{d^2c}{dt^2} = A \sin(kt)$ 
 $y = V_1$  and  $V_2 = by + \frac{b^2}{4a} + A \sin(kt)$ 
 $f(x-t) - f(a)$

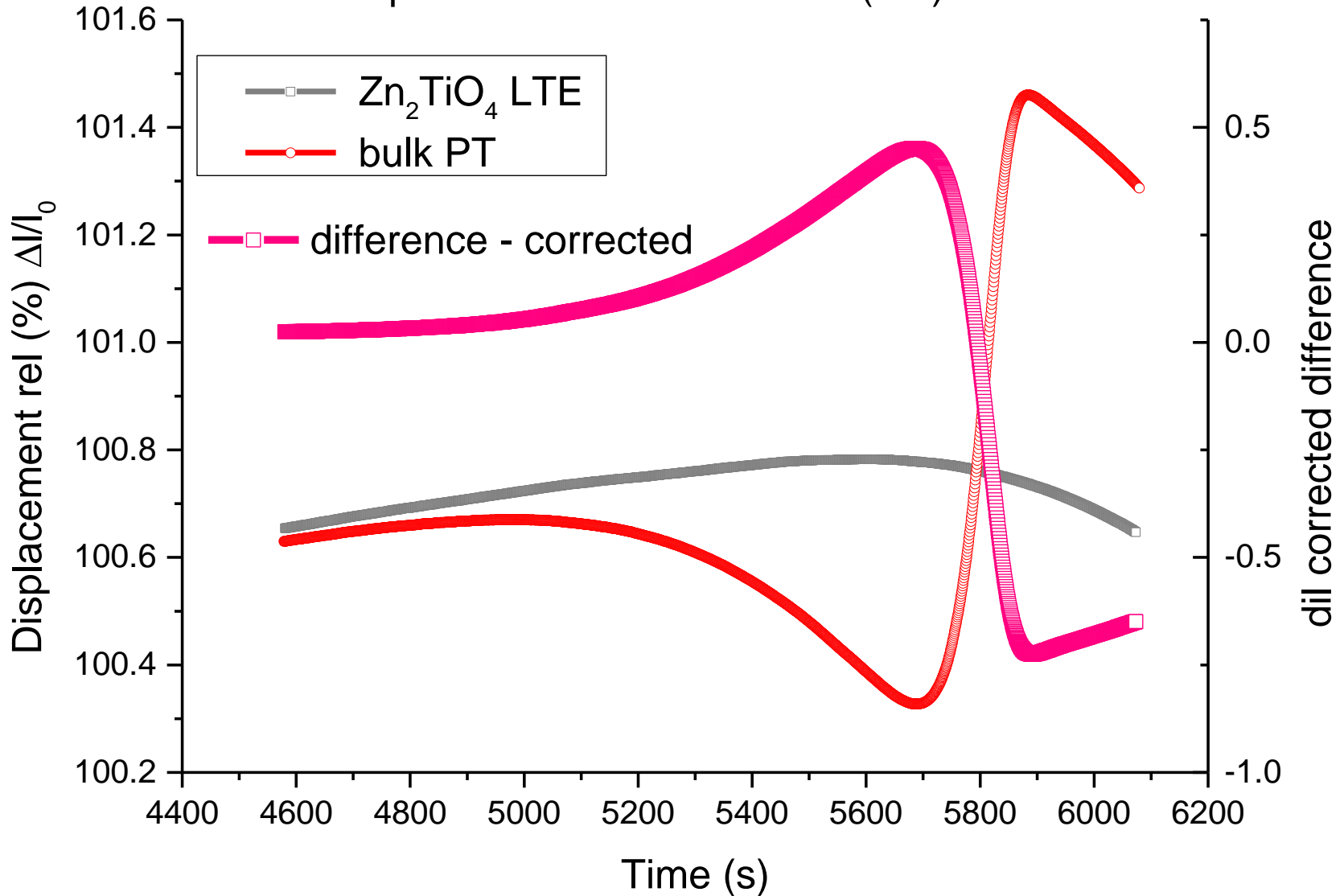
**Calculus**

Includes illustrations of a calculator, a pencil, a ruler, a protractor, and a graphing screen.

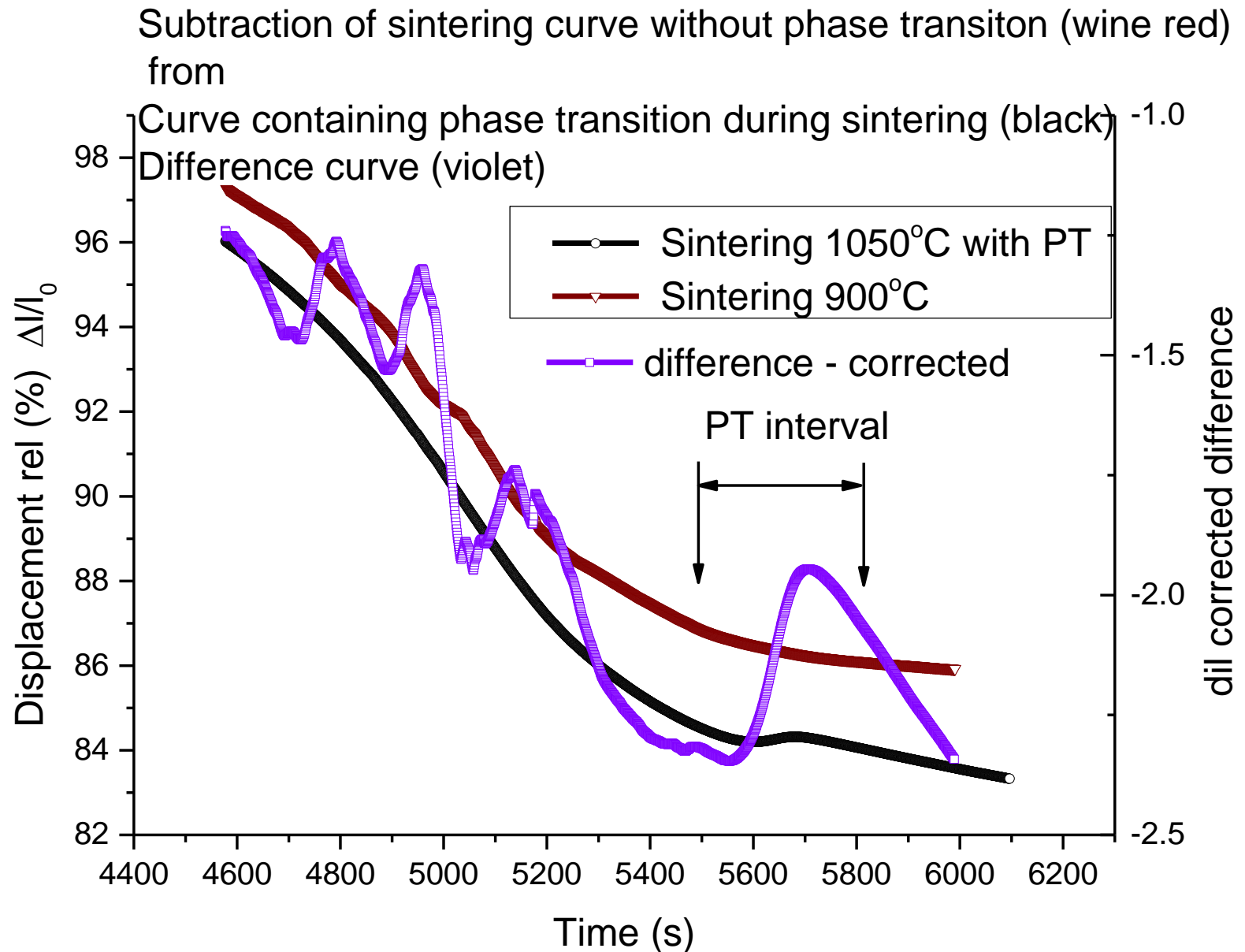


# Correction by subtraction - bulk

subtraction of  $\text{Zn}_2\text{TiO}_4$  linear thermal expansion (gray)  
from bulk phase transition dilatation (red)

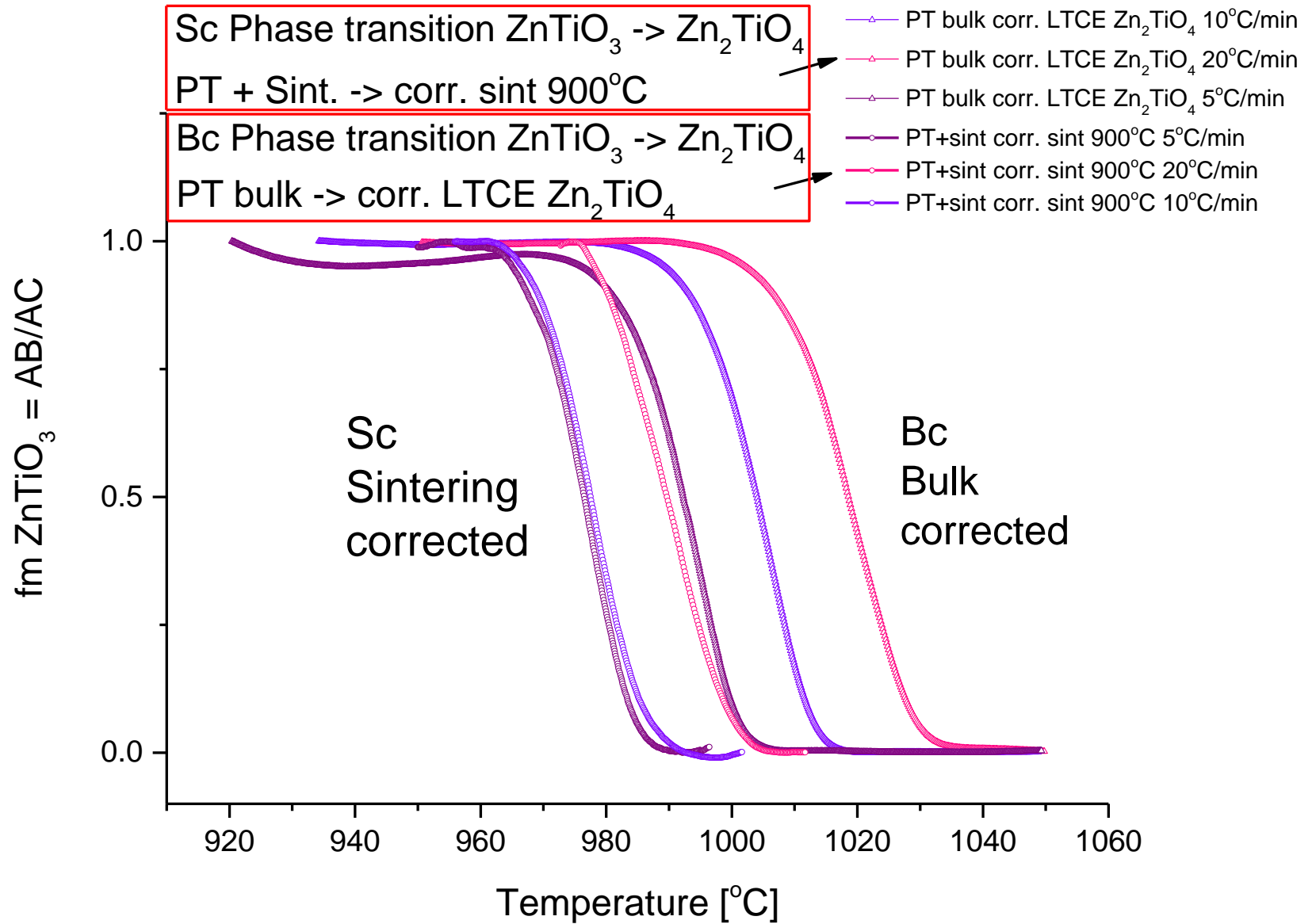


# Correction by subtraction - sintered



# Phase transition kinetics comparison:

## Corrected



# Phase transition kinetics comparison:

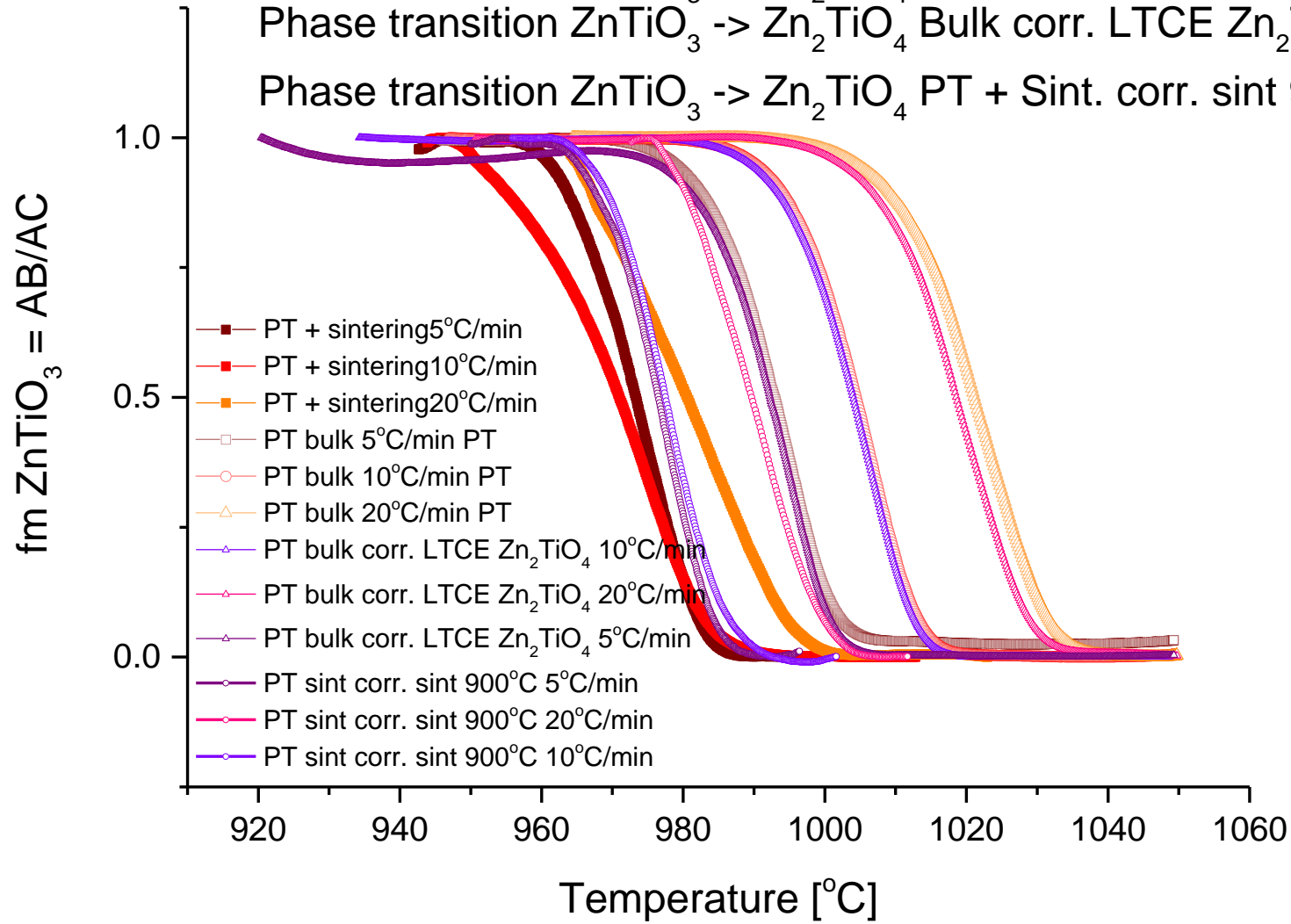
## Experimental vs. Corrected

Phase transition  $\text{ZnTiO}_3 \rightarrow \text{Zn}_2\text{TiO}_4$  PT + Sintering

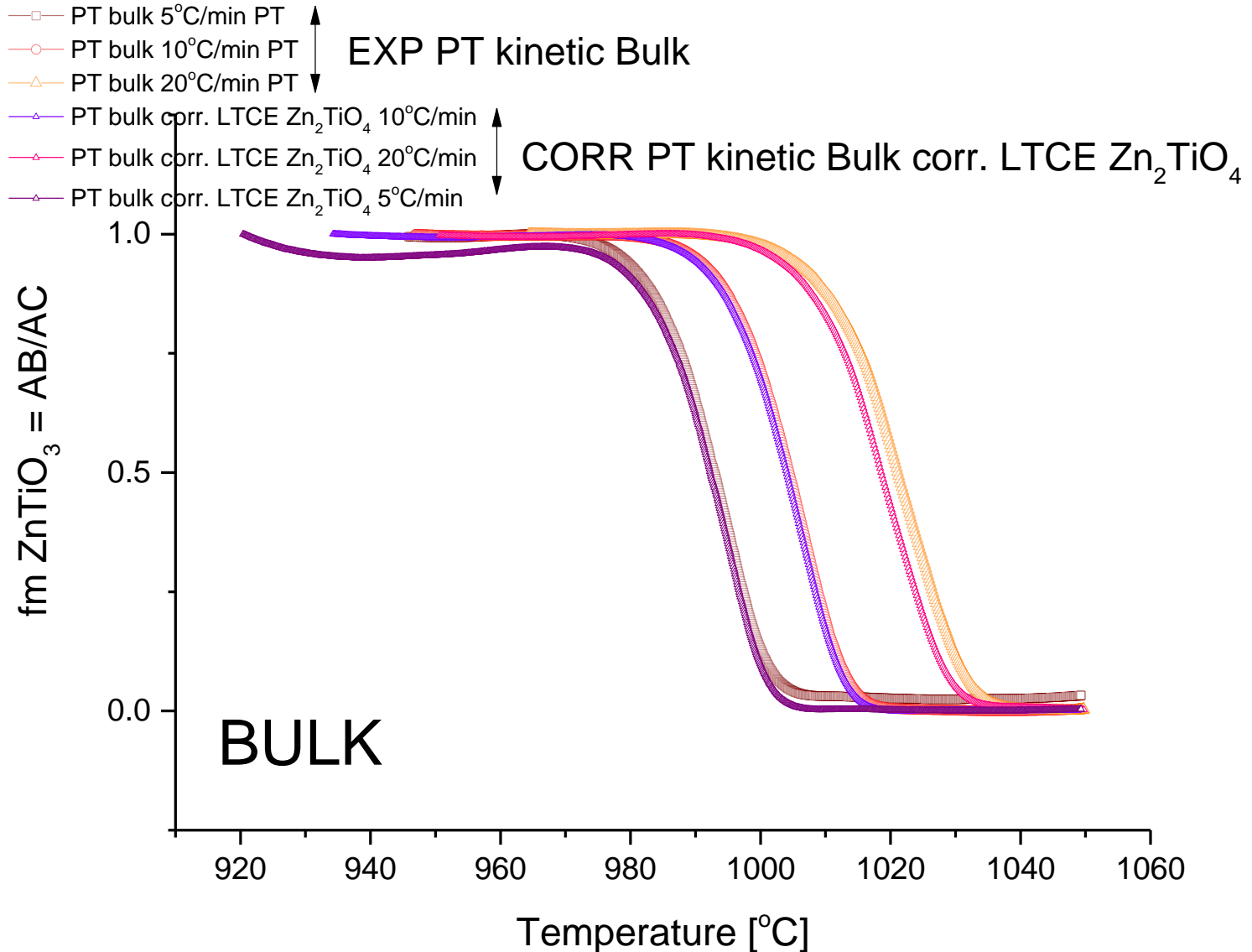
Phase transition  $\text{ZnTiO}_3 \rightarrow \text{Zn}_2\text{TiO}_4$  Bulk

Phase transition  $\text{ZnTiO}_3 \rightarrow \text{Zn}_2\text{TiO}_4$  Bulk corr. LTCE  $\text{Zn}_2\text{TiO}_4$

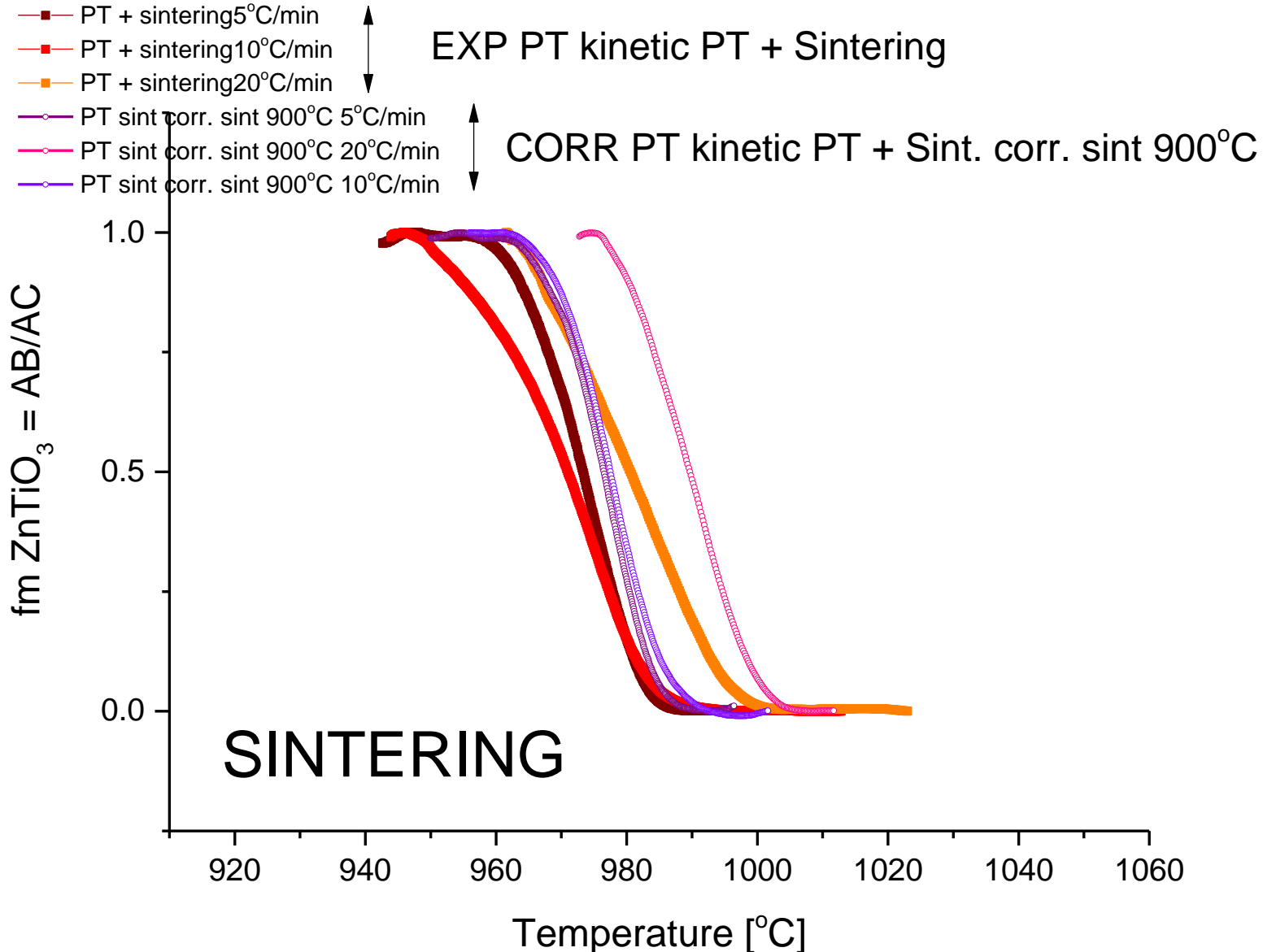
Phase transition  $\text{ZnTiO}_3 \rightarrow \text{Zn}_2\text{TiO}_4$  PT + Sint. corr. sint 900°C



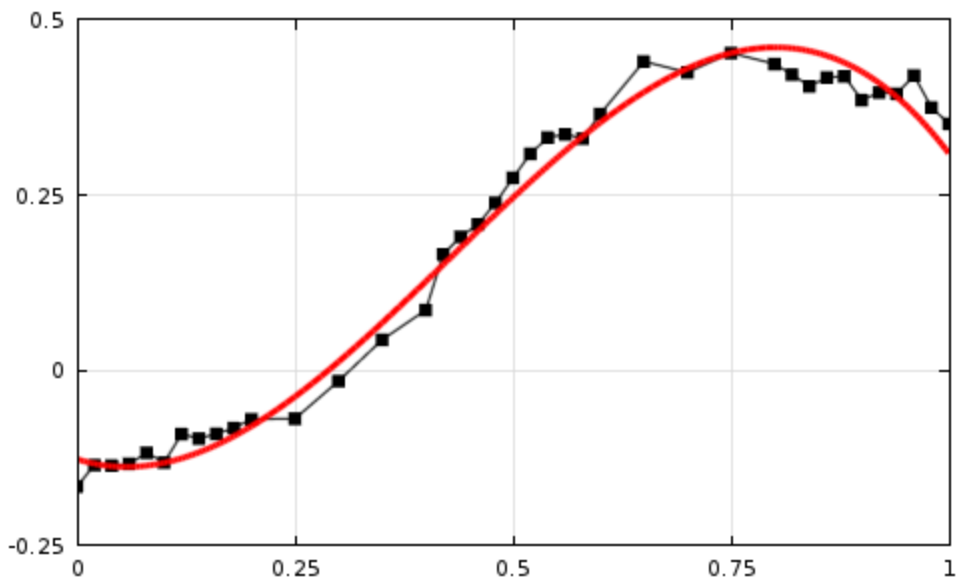
# Phase transition kinetics comparison: Experimental vs. Corrected - BULK



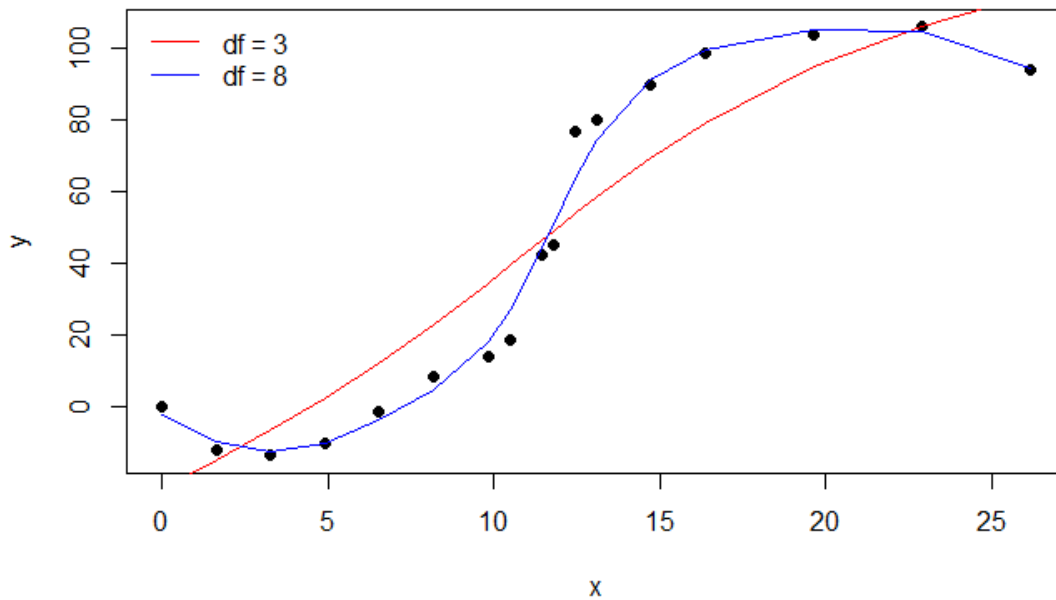
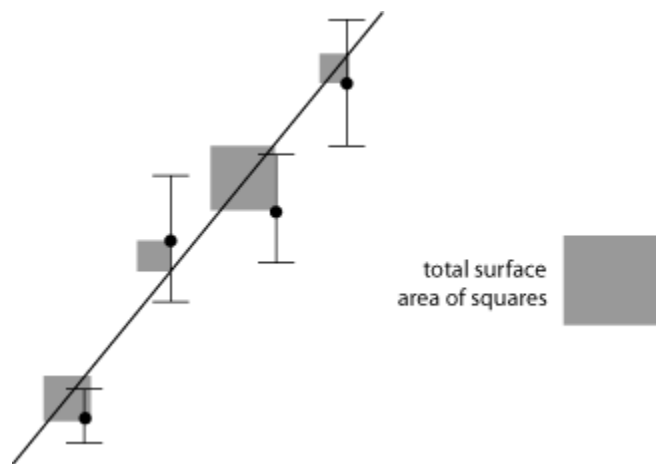
# Phase transition kinetics comparison: Experimental vs. Corrected- SINTERING



# Fitting



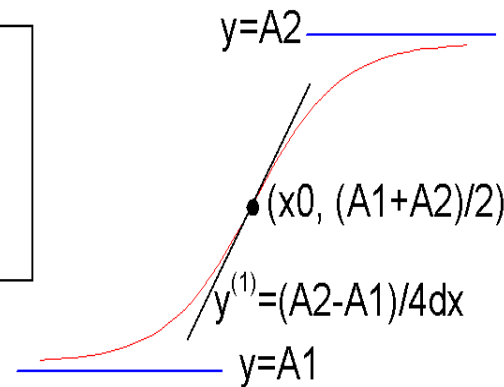
Smoothing Splines with Varying df



# Boltzmann fitting function

$$y = \frac{A_1 - A_2}{1 + e^{(x-x_0)/dx}} + A_2$$

init value:  $A_1=0$   
 final value:  $A_2=1$   
 center:  $x_0=0$   
 time const:  $dx=1$



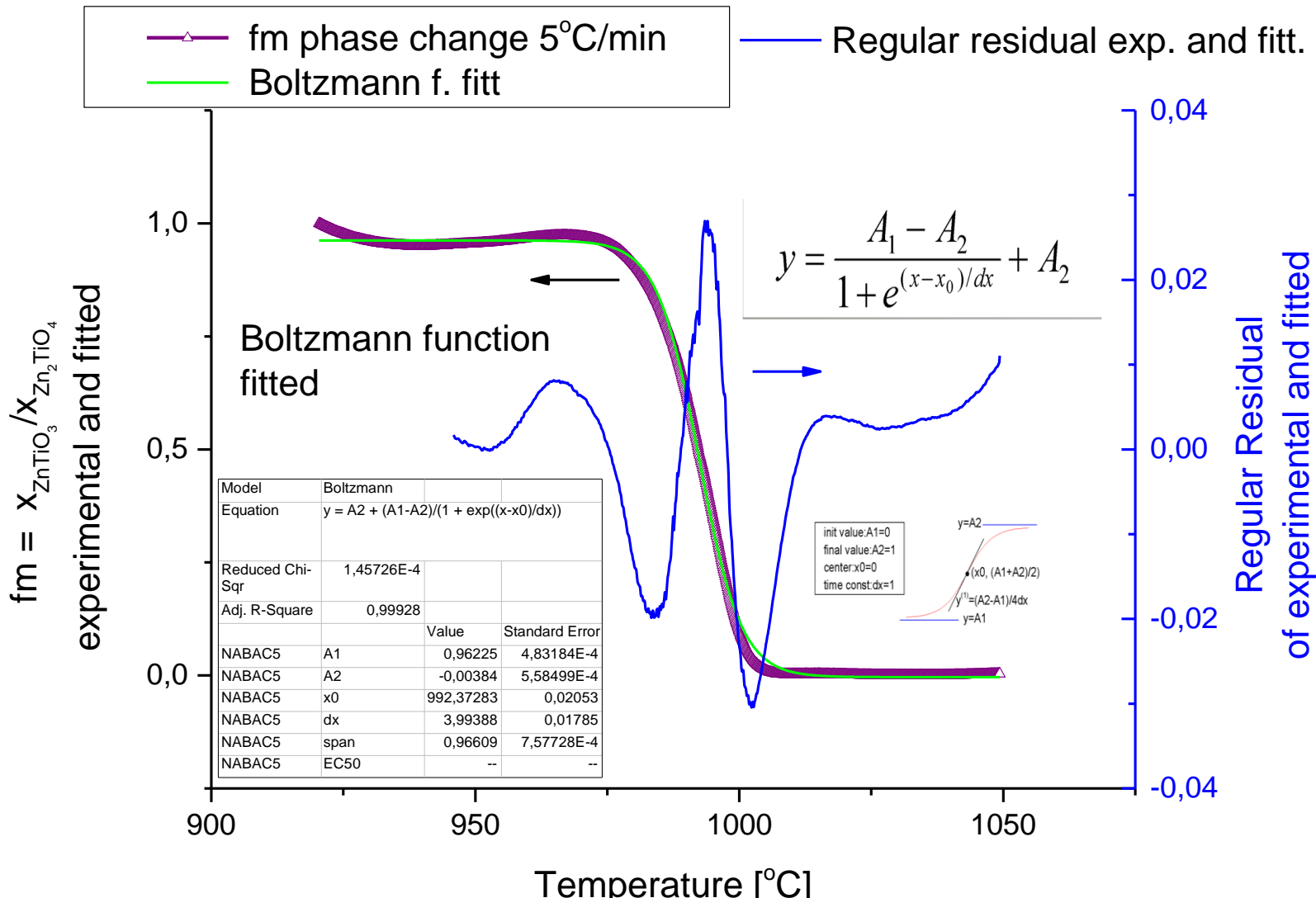
$$\frac{V^\beta(t)}{V} = 1 - \exp\left[-\frac{4\pi}{3} \int_0^t J v^3 (t-t')^3 dt'\right] . \quad \frac{V^\beta(t)}{V} = 1 - \exp\left[-\frac{\pi}{3} v^3 J_{ss} t^4\right] .$$

This is the Kolmogorov–Johnson–Mehl–Avrami (KJMA) equation.

The KJMA Eq. 11.45 predicts that the volume fraction at  $t = 0$  is zero, but has a sigmoidal shape with increasing slope that later gives way to an asymptote at long time with  $V^\beta/V = 1$ . The actual shape of  $V^\beta/V$  is typically calculated for two cases. The first



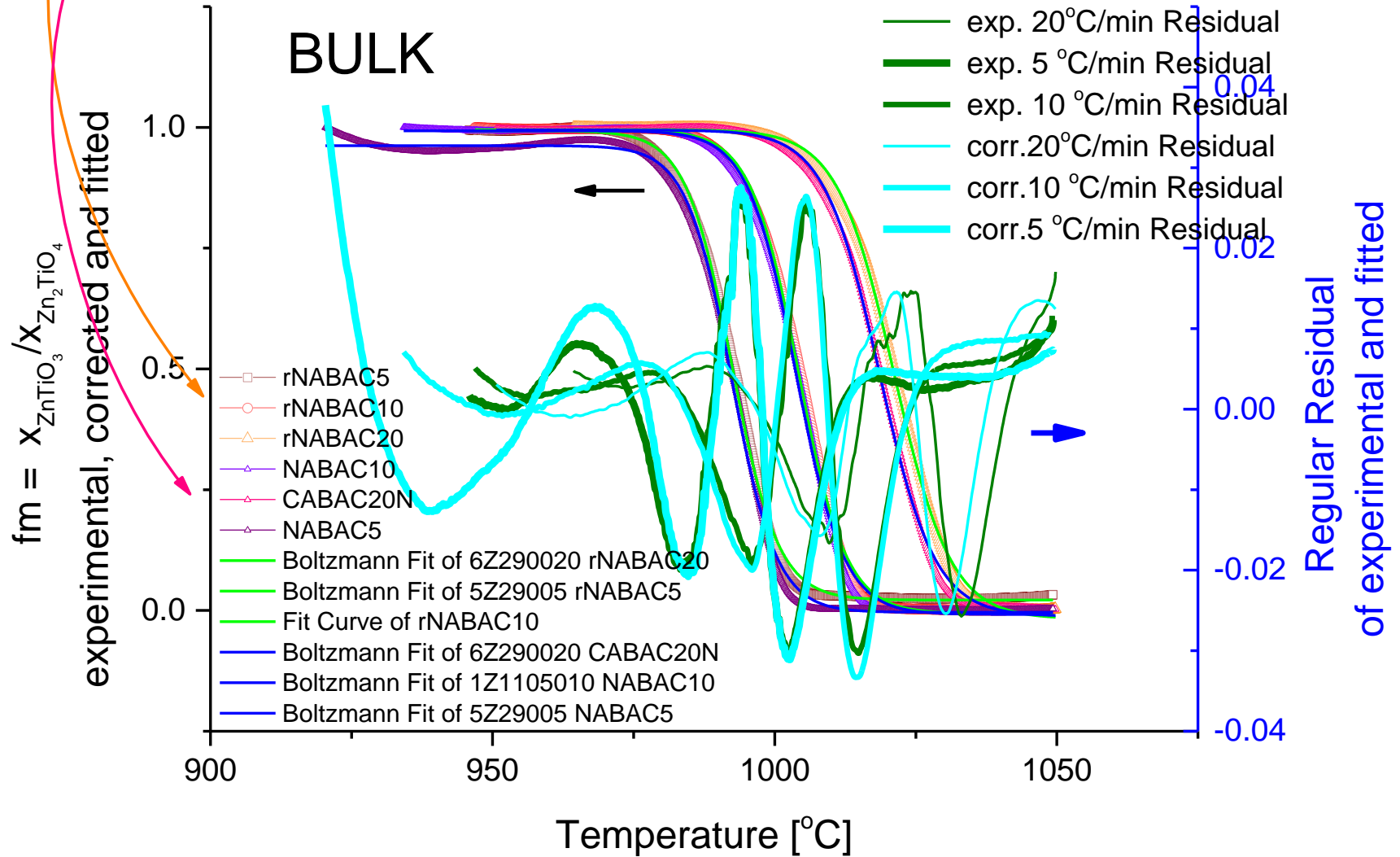
# Phase transition curve, Boltzmann fitting function – Bulk, LTEC corrected, 5°C/min



# Bulk - experimental and corrected Boltzmann function fitted – Residuals

EXP Phase transition  $\text{ZnTiO}_3 \rightarrow \text{Zn}_2\text{TiO}_4$  Bulk

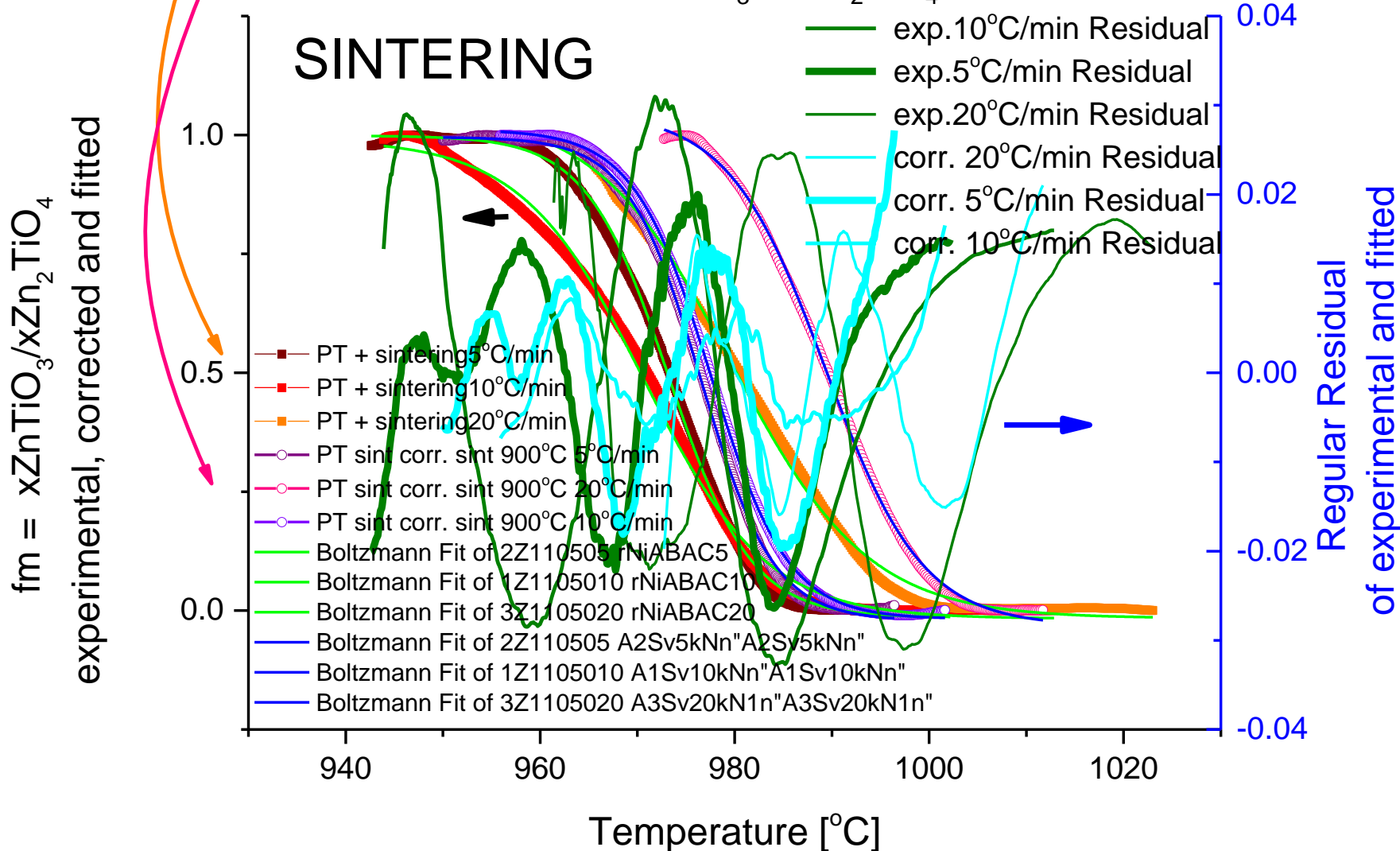
CORR Phase transition  $\text{ZnTiO}_3 \rightarrow \text{Zn}_2\text{TiO}_4$  Bulk corr. LTCE  $\text{Zn}_2\text{TiO}_4$



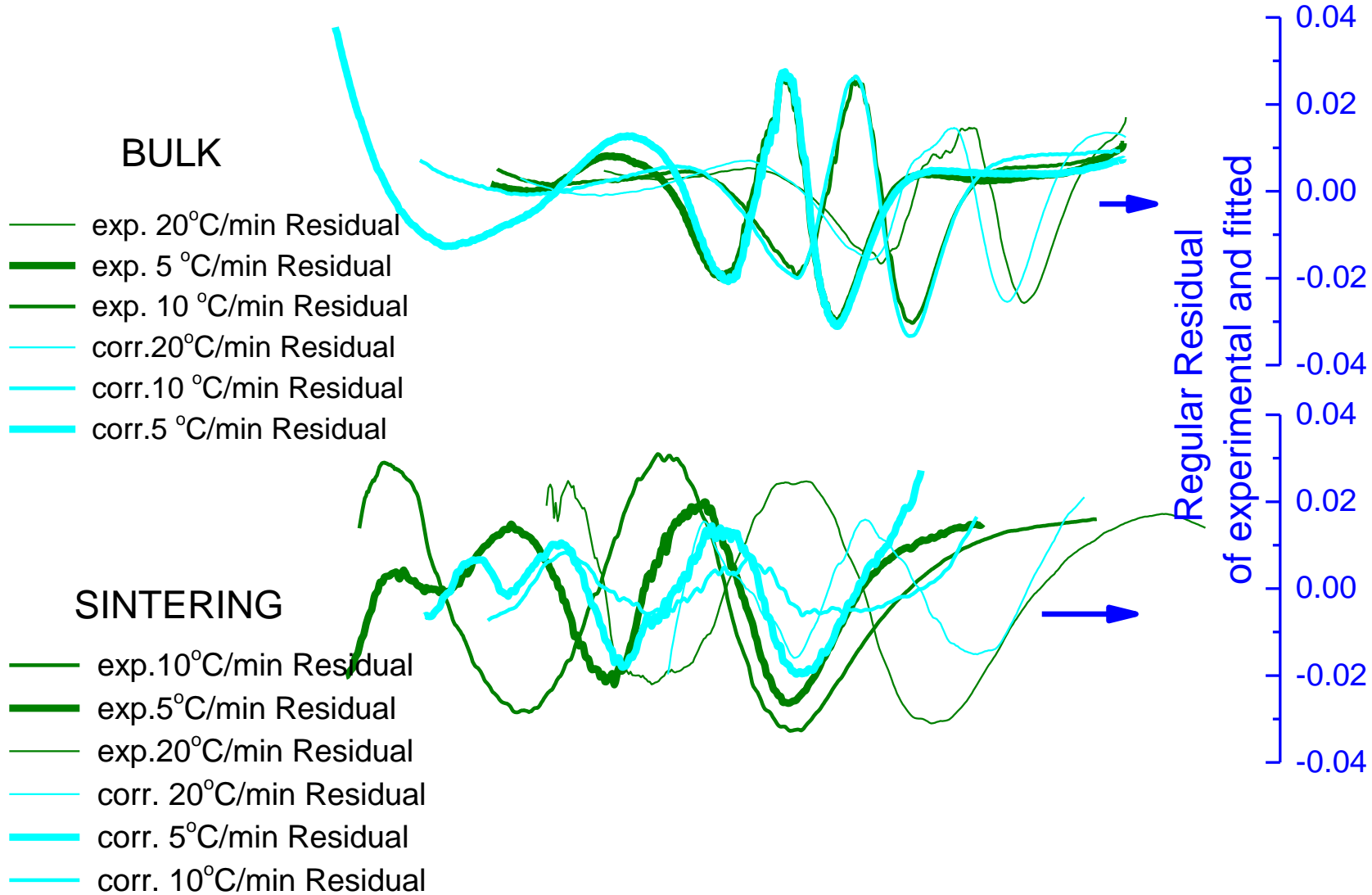
# Sintering - experimental and corrected Boltzmann function fitted – Residuals

EXP Phase transition  $\text{ZnTiO}_3 \rightarrow \text{Zn}_2\text{TiO}_4$  PT + Sintering

CORR Phase transition  $\text{ZnTiO}_3 \rightarrow \text{Zn}_2\text{TiO}_4$  PT + Sint. corr. sint 900°C



# Fitting function Residuals comparision



# Conclusion

- ✓ Phase transition for bulk specimens temperature is a function of heating rate (possible Kissinger equation usage)
- ✓ Sintering phenomenon substantially effects phase transition (temperatures are lowered by simultaneous sintering)
- ✓ Correction by sintering submission does not affect temperatures of the phase transition (although kinetic of the phase transition is different)
- ✓ Phase transition kinetics from dilatograms by lever`s rule is most prommsing (softvare obtained with dilatometric device does not includes this option)

THANK YOU FOR  
YOUR PATIENCE  
AND ATTENTION.

